

GHz QKD at telecom wavelengths using up-conversion detectors

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Abstract. We have developed a hybrid single photon detection scheme for telecom wavelengths based on nonlinear sum-frequency generation and silicon single-photon avalanche diodes (SPADs). The SPAD devices employed have been designed to have very narrow temporal response, i.e. low jitter, which we can exploit for increasing the allowable bit rate for quantum key distribution. The wavelength conversion is obtained using periodically poled Lithium niobate waveguides (W/Gs). The inherently high efficiency of these W/Gs allows us to use a continuous wave laser to seed the nonlinear conversion so as to have a continuous detection scheme. We also present a 1.27 GHz qubit repetition rate, one-way phase encoding, quantum key distribution experiment operating at telecom wavelengths that takes advantage of this detection scheme. The proof of principle experiment shows a system capable of MHz raw count rates with a QBER less than 2 % and estimated secure key rates greater than 100 kbit/s over 25 km.

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1. Introduction

The speed with which quantum key distribution (QKD) has progressed in recent years has been remarkable. From the original idea in 1984 [1], to the first key exchange in 1992 [2] and then outside the lab by 1995 [3, 4], to commercial fruition in 2001 [5], only 20 years have passed. Unfortunately the speed of the actual key exchange remains quite slow. We have seen some advances towards faster QKD with clock synchronisation over 1 GHz already achieved [6, 7]. In both of these cases attainable distance was limited by the choice of wavelength and the rate of the quantum channel was limited by a relatively wide detector response (i.e. fairly large timing jitter). Further progress has also led to the realisation that single or two photon sources are not required for security, and that weak pulses suffice. There have also been other more fundamental attempts to find different protocols that allow for an increase in the quantum communication rates for weak pulse schemes like decoy state QKD [8, 9, 10], the SARG protocol [11], and the protocol recently proposed by Stucki *et al.* [12].

Our goal is to increase the QKD rate for telecom wavelengths. To this end, we exploit planar Silicon (Si) SPAD devices [13, 14] with very low timing jitter, of the order of 40 ps, that are capable of MHz regime photon counting and have low noise and afterpulse probabilities. This first of all requires that we convert from telecom transmission wavelengths to the Si detection band. To achieve this we use nonlinear sum-frequency generation (SFG), or up-conversion in a periodically poled Lithium niobate (PPLN) waveguide (W/G). Takesue *et al.* [15] have recently incorporated a similar detection scheme into differential phase shift QKD, increasing both rate and distance for secure QKD, though using standard Si SPAD with larger timing jitter, of the order of 400 ps and more [6, 7]. By incorporating the low jitter SPADs in the experimental apparatus we can further increase the secure bit-rates and obtain greater levels of stability for interferometric based schemes. What we show in this article is that whilst there are important limitations for the optics, these do not restrict us from making significant increases in the quantum bit rate for long distance (telecom wavelength) QKD with a careful choice of system parameters and components.

This article is organised in the following manner. We first introduce the basic scheme used to perform weak pulse phase encoding QKD. We then briefly describe the two different Si SPADs that we have used before we discuss the results of a wavelength conversion process for single photon detection of telecom wavelength photons. The combined characteristics of these Si-SFG detectors are then highlighted in a proof of principle experiment where they are utilised in a 1.27 GHz one-way QKD set-up.

2. Fast phase encoding QKD

We wish to implement weak pulse phase encoding QKD for both BB84 [1] and SARG [11] implementations where both have quantum and classical channel repetition rates of 1.27 GHz. We first present a general view of the experimental set-up, as shown in

If we now look at the detection system, we note that the W/Gs that are used for the SFG are polarisation sensitive, i.e. the process requires that the input photons have a specific polarisation with respect to the optic axis of the detection set-up, as we will see. This could be seen as a down side, but if we need to control, in part, the polarisation of the input signal, we might as well do it before the interferometer as after it! By using polarising beam splitters (PBSs) at the exit and the entrance of Alice and Bob's respective interferometers, we ensure that all signal photons arrive in coincidence with the clock signal in the same way that is done for the Plug&Play scheme [16] and at the same time optimising the detector's efficiencies. Another subtle technical point that should be mentioned here when comparing these two approaches is that we do not need to consider extra loss for Bob if we add a phase modulator. One can simply balance the probability amplitudes, as we have done here, with the PC and PBS at the entry to Alice's interferometer such that the combined probability amplitudes for both interferometers are equal, i.e. the loss due to the PM is compensated.

There are several elements to this experiment that are advantageous for performing rapid QKD. The laser is mode-locked to provide not only a high repetition rate and photon extinction levels, but also the appropriate width, Fourier transform limited, pulses. The optical pulse width is perhaps the most crucial parameter limiting the repetition rate. The interferometers are made from polarisation maintaining fibre and have optical path length differences of 300 ps. This extremely short time difference means that the interferometers are inherently more stable than most previous implementations (usually several ns) [3, 17]. This has been made possible due to the use of this detection scheme based on nonlinear W/Gs and silicon (Si) SPADs with very low temporal jitter. We will now discuss in more detail each of these elements and how they contribute, starting with the detection system.

3. Si-SFG single photon detectors

The idea of using SFG to facilitate a measurement in a bandwidth with better detection characteristics is not new [18]. However, it is only with recent technological advances that this approach is being revisited to study the single photon detection regime for telecom wavelengths, as well as for longer wavelengths such as $4\mu\text{m}$ [19]. In the telecom band, there are now several groups investigating this approach using commercially available single photon counting modules (SPCM-AQR), based on Si SPADs with both bulk and waveguiding PPLN crystals and either continuous or pulsed pump sources [20, 21, 22]. Whilst initial results have been promising, with respect to overall efficiencies, there have been significant problems with noise which we have not escaped either and will return to momentarily. More recently we have also seen experiments that have used this process but focused on the coherence of this conversion in the context of a quantum interface [23]. All of these schemes so far have incorporated standard Si SPADs with photon-timing jitter of the around 300-500 ps. We have studied a combination of PPLN W/Gs [HC Photonics] and two different types of Si SPADs with low timing jitter. The

overall goal is to develop a compact and practical single photon detection system for telecom wavelengths with low noise, high temporal resolution and a quantum efficiency comparable to current InGaAs SPADs.

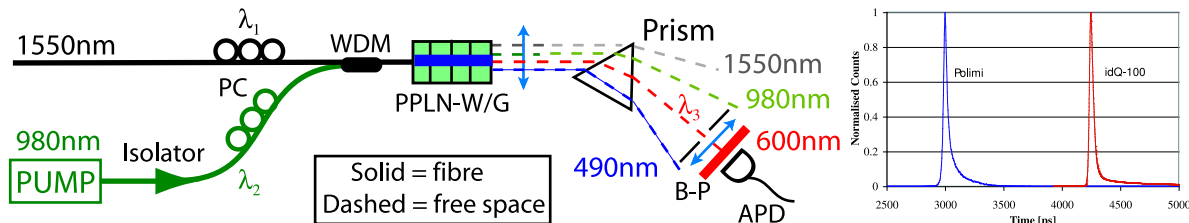


Figure 2. (Left) Schematic of the Si-SFG hybrid detection scheme using PPLN waveguides and Si SPADs. (Right) Timing jitter for the two SPAD used. See text for details.

Usually when working with SFG one operates in a regime where there are many photons. Here we go to an extreme where we are really interested in converting a single photon from one wavelength to another using a pump at a third wavelength to aid, or seed, the process. The energy conversion process that we are interested in is $1550\text{ nm} + 980\text{ nm} \rightarrow 600\text{ nm}$. Because of the high conversion efficiency of these W/G devices [18], we can use standard, and relatively inexpensive, 980 nm diode lasers [JDS Uniphase]. This allows the Si-SFG detectors to be operated in a continuous mode. Whilst we don't foresee any problems for SFG at the single photon level, due to the high pump powers we are using here, there are other processes that can introduce noise to the overall process as we will discuss momentarily. Figure 2 shows the experimental arrangement for the detectors. A single photon at 1550 nm is mixed with a large flow of 980 nm pump photons at a wavelength division multiplexer (WDM). The polarisation controllers (PC) ensure that all photons enter the PPLN W/G with the correct polarisation. The WDM is pigtailed to the W/G input. The free space output is then collimated and passed through a dispersion prism to spatially filter the unwanted spectral components. After the W/G there is still a large flow of 980 nm photons as well as 490 nm photons that are generated by second harmonic generation (SHG) from the pump. It is crucial to filter these as the SPADs are relatively efficient at these wavelengths. The signal at 600 nm is then focused through a bandpass filter (600-40 nm) and onto the SPADs.

SPAD devices for accurate single-photon timing have been under development for many years at Politecnico di Milano (Polimi) resulting in various generations of silicon planar CMOS (Complementary Metal Oxide Semiconductor) compatible technology [24]. Their capability of photon timing with jitter down to 20 ps has been demonstrated [13] and the concurrent progress in electronics for the detector operation (integrated Active Quenching Circuit iAQC) have made it possible to develop compact single photon timing modules [25]. More recently, Rochas *et al.* were able to design and fabricate SPAD devices in an industrially available silicon high-voltage CMOS circuit technology

[14]. Both these SPADs [idQuantique id100 and Micro Photon Devices PDM20T] have features suitable to our purpose and have been employed in the experimental tests. They both exhibit timing jitter of 40 ps, dark counts of less than 200 Hz with peak detection efficiencies in the blue/green spectral range with an active area with 20 μm diameter and afterpulse probabilities of 1 % at room temperature. The timing jitter for both of these devices is shown on the right of figure 2.

The SFG conversion efficiency can be shown to be $\eta = N_3/N_1 = \sin^2[(\eta_{\text{norm}}P_2)^{1/2}L]$ [21]. Here N_1 is the number of 1550 nm input signal photons and N_3 is the 600 nm output signal photons for detection. P_2 is the input power at 980 nm and η_{norm} is a normalised internal conversion efficiency of the W/G. This is an idealised solution, which can reach 100%, though in reality, for the overall efficiency, we need to consider coupling losses and internal transmission losses such that the conversion efficiency will be limited, in our case to around 30-35%. Finally we need to include filtering and the efficiency of the Si SPAD itself, which will further reduce the overall detection efficiency.

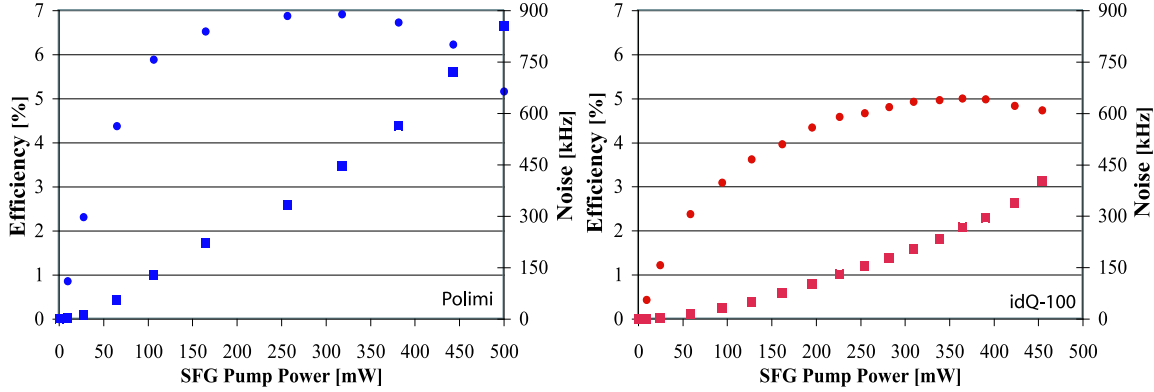


Figure 3. The overall detection efficiency (circles) and noise response (squares) as a function of the input pump power. (Left) Polimi Si-SPAD. (Right) idQ Si-SPAD.

To characterise the detectors we first look at this conversion efficiency and noise as a function of the input pump power P_2 at 980 nm. To do this we have used a set-up as depicted in figure 2 with two calibrated variable attenuators to reduce the 1550 nm signal down to the single photon counting regime [26]. The results for both W/G-SPAD combinations under test are shown in figure 3. We find peak detection efficiencies of around 5-7% which is in good agreement with the theory given the conversion, filtering and detection characteristics for each set-up. We note that the efficiency reaches a peak and then starts to degrade as the pump power increases. This is the normal response of this type of process where we have so many photons at 600 nm that it becomes efficient to reconvert them back to 1550 nm, i.e. the inverse process of parametric down-conversion (PDC).

We also see the noise characteristics for these Si-SFG detectors is not only significant but nonlinear as a function of the pump power. The noise is measured concurrently with the efficiency by blocking the input signal and is simply the number of detection events

one obtains without an input. Whilst one would expect the large number of pump photons could contribute, as the SPADs are still sensitive at these wavelengths, suitable filtering can remove this. The response for this should also be linear, but here there is clearly a nonlinear component that is not normal. A further study as to the origins of this noise is currently underway as there are several possibilities. Fluorescence and Raman scattering have already been suggested in similar experiments [20, 21, 22]. We would also like to put fourth another possibility for the case of PPLN crystals and specifically W/Gs.

Phase matching for different processes in PPLN W/Gs is achieved by changing the size of the poling periods [27]. As mentioned previously, SFG is the inverse of PDC, and we have also observed SHG in these W/Gs, so we can start to imagine a large family of possible conversion processes. One allowable process is for PDC, where the 980 nm pump generates photon pairs at 1550 nm and 2665 nm. This 1550 nm photon can then in turn be converted to 600 nm which would produce a quadratic noise response, as we see. Unfortunately we cannot tune to another wavelength as the 2665 nm photons are not guided, but emitted into the W/G substrate. In doing this they can satisfy Cerenkov phase matching conditions which results in a broad band generation of photons around 1550 nm [28] which we could observe experimentally.

In our case we are interested in QKD and as such the efficiency-noise relationship is fundamental. Even though we have relatively high levels of noise we find, with both W/G-SPAD combinations, that we can reduce the efficiency to around 2% with less than 20 kHz of noise. We can then take further advantage of the low jitter of the SPADs, as illustrated on the right of figure 2, by working with detection windows of only a few hundred ps. If we do this, we see that we have an effective noise probability per gate which is comparable with current InGaAs SPADs, though we now have a detector that can operate in the MHz counting regime.

4. The chromatic dispersion limit - Fourier transform limited source

We have overcome several problems on the detection side with the Si-SFG detectors, so now let us look at the optical pulses. We need to have relatively short pulses to take advantage of the temporal resolution the SPADs provide. However, we will be using fiber optic transmission and as such chromatic dispersion needs to be carefully considered [29]. Chromatic dispersion in standard optical fibers at 1550 nm is around $17 \text{ ps nm}^{-1} \text{ km}^{-1}$. There is a spectral bandwidth between 80-200 pm, that provides transform limited pulses of 40-100 ps, that is ideal for transmission up to 50 km in fibre. Otherwise, one either starts with pulses that are too short and quickly have extremely large pulse widths due to chromatic dispersion, or we simply start off with pulses that are too large to take advantage of our small jitter SPADs. This is a difficult regime in which to find telecom wavelength lasers that are both, in the GHz repetition range, and have short, but not too short, pulses.

In this instance we have chosen to work with a custom made mode-locked telecom

wavelength (1550) laser operating at a repetition rate of 1.27 GHz (Ultrafast laser physics group, ETH Zurich). There are many compelling reasons to use a pulsed laser directly as an optical source in telecommunications systems, both classical and quantum. First, this eliminates the need for a modulator to create the pulses and thereby can simplify system architecture. Secondly, the extinction ratio of pulsed lasers is typically very good and much higher than for modulated cw sources improving the system signal-to-noise ratio. Furthermore, the pulses produced are transform limited and hence present a much better proposition for fibre optic transmission. Passively mode-locked, diode pumped solid-state lasers have been presented with repetition rates up to 50 GHz around 1550 nm [30], and up to 80 GHz in the 1 μ m wavelength region [31]. With novel pump diodes a previously demonstrated 160 GHz laser could also easily be extended to diode pumping [32].

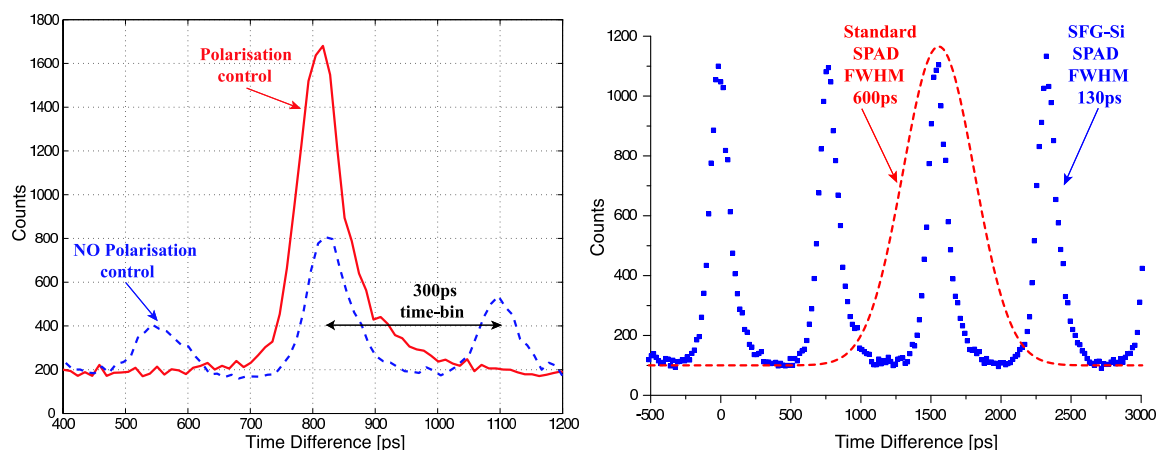


Figure 4. (Left) Time difference histogram showing the effects of controlling the polarisation to remove the satellite peaks. (Right) Extended view of a train of pulses highlighting the side peak extinction and the superior temporal resolution one would expect with respect to standard Si-SPADS.

The laser used in this experiment has an Er:Yb:glass gain medium that is pumped by telecom-grade 980 nm laser diode, which typically delivers 300 mW of pump power in a diffraction-limited beam. Most of the pump radiation is absorbed by the ytterbium dopant and then transferred to erbium ions, generating gain in the 1550 nm region. Passive mode-locking is achieved by placing a semiconductor saturable absorber mirror (SESAM) at one end of the cavity [33, 34, 35]. An intracavity etalon is included to adjust the laser wavelength and to set the pulse duration to the desired value. Typical pulse durations are in the range of 1 ps up to nearly 20 ps, while the average output power is around 10 mW. Further external spectral filtering [AOS fibre Bragg grating - 100 pm] is used which corresponds to Fourier transform limited pulses of around 80 ps.

5. Proof of Principle for rapid QKD

Let us now look at the first proof of principle results. The time-of-arrival histogram on the left of figure 4 illustrates the type of signal with which we are dealing. This figure shows the two cases, where the polarisation is controlled, or not, before entering Bob's interferometer. We see that when the polarisation is controlled the satellite peaks (non-interfering short-short and long-long events for the interferometers) can be made to disappear. We control the polarisation between the two interferometers with a polarisation controller (PC), also illustrated in figure 1. This approach reduces the noise level due to pulses spreading into adjacent time-bins. If we do not control Bob's input polarisation and the channel is completely depolarised, the count rate is reduced to its normal level, i.e. we have all three peaks and reduce the bit rate by a half.

We note here that the histogram is generated with start and stop signals given by the two SPADs and not with one SPAD and the clock. This is due to the clock being too fast for the available time-to-amplitude converter [Tenelec TC863]. As such the FWHM of these peaks includes the contributions from both SPADs, the optical pulse, and all of the associated electronics. It is important to note that the following measurement data, for the QKD, is generated independently to this and corresponds to coincidence events between the clock and each of the SPADs. These widths govern both, how quickly we can send successive pulses and how large the path length difference can be in the interferometers. Even in an extended view of the pulse train that we are using, as shown on the right of figure 4, we see that the pulses are clearly defined and that the side peaks are suppressed. Furthermore, at 25 and 50 km we only observe a broadening of these histogram peaks of around 40 to 80 ps respectively, as expected. The dashed curve with a FWHM shows the type of response we would expect from a standard Si-SPADs.

In this proof-of-principle experiment we have not sent random bit trains but simply the same bit many times. Measurements were made with two different lengths of fibre, 25 km and 50 km. In this first instance our goal is to highlight the advantages of the timing jitter and count rates afforded by the SFG-Si SPADs. Therefore, for each run, we set the phase, take an average, then set the next phase. The raw data for a series of these measurements is shown in table 1. The results are shown for each detector (D_1 , D_2) and are averages over a one minute interval, for two different states which are defined by Alice's choice of phase. The first value in each case, either result "0" or result "1", being the correct or True (T) value, followed by the wrong or False (F) value. We clearly see the advantages of using the SFG-Si detection scheme as it is now possible to have count rates R of over 2 MHz.

We now need to think about the QBER. The QBER is simply the ratio of false events to the total number of events after sifting (reconciliation) and for the two cases we find,

$$\begin{aligned} \text{QBER(BB84)} &= \frac{(1/2)(P_{opt}P_{phot}+P_{dark})}{(1/2)(P_{phot}+2P_{dark})} \approx P_{opt} + \frac{P_{dark}}{P_{phot}} \equiv Q_{opt} + Q_{det}, \\ \text{QBER(SARG)} &= \frac{(1/2)(P_{opt}P_{phot}+P_{dark})}{(1/4)((1+2P_{opt})P_{phot}+4P_{dark})} \approx 2P_{opt} + 2\frac{P_{dark}}{P_{phot}} \equiv 2(Q_{opt} + Q_{det}), \end{aligned} \quad (1)$$

Table 1. Raw data for the coincidences (SPAD + Clock) for the 2 protocols and two distances (25 and 50 km). See text for details.

	True / False	BB84-25	SARG-25	BB84-50	SARG-50
"0"	D ₁ (T) / D ₂ (F)	763 k / 11.6 k	2.24 M / 17.9 k	117 k / 9.54 k	636 k / 12.1 k
"1"	D ₂ (T) / D ₁ (F)	660 k / 14.5 k	1.84 M / 19.3 k	104 k / 11.5 k	558 k / 16.9 k

where $Q_{opt} = (1 - V)/2$, ($V \sim 1$ being the visibility). We have also assumed that $P_{dark} \ll P_{phot} = \mu \eta t \ll 1$. As we initially said, there are two possibilities for Bob, one interferometer and two detectors or two interferometers and 4 detectors. The two cases do not give the same results, so it would be interesting to see how this varies for the two different protocols. In the case of four detectors we find that the component Q_{det} increases by a factor two. It must be remembered that Q_{det} is calculated using the optimal μ for each protocol, so things may not appear to be as big a problem for SARG as one might first think. The theory uses the following experimentally verified values, $Q_{opt} \approx 0.5\%$, a detection efficiency of 1.2% and a detector dark count probability $P_{dark} \approx 7 \times 10^{-6}$ per gate. The gate width is defined by the electrical pulse widths of the clock and the Si-SPAD signals which are around 300 ps. The experimental QBER is calculated simply as the average number of wrong counts divided by the average number of total counts for both detectors (using the results in table 1), with an extra factor of two in the case of SARG to account for the greater sifting losses.

Once we have determined the errors we can then think about estimating the secure key rate R_{sk} that we could expect. Firstly, to do this we need to be clear about the assumptions that we are using to analyse the security of the system. Obviously this is a weak pulse encoding scheme, and we assume we are working in a trusted device scenario where Eve doesn't have access to the detectors, i.e. she cannot change Bob's detector efficiencies or dark counts. In this instance we are not considering coherent attacks, and as such, Eve only performs individual attacks, or photon number splitting attacks when there are two or more photons per pulse. The reduction in the raw key rate for both cases scales as,

$$R(1 - H(QBER) - I_{Eve})P_{sift} \quad (2)$$

where H is the Shannon entropy, I_{Eve} is Eve's information, and $P_{sift} = 1/2$ for BB84 [36] and $1/4(1 + Q_{opt} + 2Q_{det})$ for SARG [37]. Eve's information reduces to $I_{Eve} \approx \mu/2t \approx 1/2$ for BB84 [36], and $I_{Eve} \approx I_1 + (1 - I_1)\mu^2/12t \approx 0.6$ for SARG, where $I_1 \approx 0.4$ [37]. In each case the optimal μ (mean number of photons per pulse) is used, BB84 where $\mu_{opt} = t$, and SARG where $\mu_{opt} = 2\sqrt{t}$ ($t \equiv$ transmission). For a detailed discussion concerning the security of these schemes, the reader is referred to [36] for BB84 and [37] for SARG.

In table 2 we see the average results for the raw bit rates, the QBER and an estimate of the secret key rate, given R and the QBER, for the case of one interferometer and two detectors. The good correspondence between the QBER for theory and

Table 2. Results for GHz QKD for two different fibre lengths using both BB84 and SARG protocols. R = raw key rate, S = secure key rate.

Protocol	km	μ	R [Bit/s]	QBER(exp) [%]	QBER(th.) [%]	S [Bit/s]
BB84	25	0.286	710 k	1.84	1.56	135k
SARG	25	1.064	2.04 M	1.82	1.62	140 k
BB84	50	0.101	110 k	9.51	9.21	2k
SARG	50	0.640	590 k	4.71	4.11	20k

experiment implies that the error due to chromatic dispersion effects is minimal, indeed a $Q_{disp} \approx 0.3\%$ for the 50 km transmission would bring the two inline. Whilst with this set up we are capable of performing QKD using either protocol over these distances, there are definite advantages to using SARG. At 25 km we have a raw count rate of over 2 Mbit/s for SARG compared with 710 kbit/s for BB84, both with similar QBER. At this distance there is not a great difference in terms of the QBER or final secret key rate. However, at 50 km we have 590 kbit/s and 110 kBit/s respectively, and whilst the QBER for BB84 has increased significantly, and hence we extract only a relatively small amount, SARG still has a respectable QBER of less than 5 %, and we estimate a secure key rate of around 20 kbit/s, an order of magnitude improvement.

6. Conclusion

We have presented two primary results, a SFG-Si telecom single photon detector that has low jitter and is capable of MHz count rates, and a GHz QKD system that is optimised to use this detection scheme. The Si-SFG hybrid detector has a single photon detection efficiency of over 5%, though with a significant noise problem. This requires further study to determine to what level this noise problem can be minimised. However, as it stands the temporal resolution and afterpulse effects are better than standard InGaAs APDs for telecom wavelengths and we can also use these detectors in a continuous, or free running, mode. The phase encoding QKD scheme has been shown to work over distances of 25 km and 50 km of standard telecom fibre. Importantly, these results show that the bit rate for long distance QKD can be substantially increased before there are any significant optical restrictions. The system has shown that it is capable of MHz raw bit rates and estimated secure key rates greater than 100 kbit/s over distances of 25 km and 20 kbit/s over 50 km. Indeed, with a foreseeable reduction in detector noise, and minor increases in detection efficiency, high secure rates up to distances of 100 km should be possible.

Acknowledgments

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